Methods for prediction of aircraft turbulence and their validation

FISAPS Workshop 30 Aug-1 Sep 2023

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"This research is in response to requirements and funding by the Federal Aviation Administration (FAA). The views expressed are those of the authors and do not necessarily represent the official policy or position of the FAA. NCAR IS sponsored by the National Science Foundation."

Aviation turbulence - Motivations

- Economic cost of ~ \$200M/yr
- Accounts for 75% of air carrier accidents
- ~ 15 serious injuries, ~50 minor per year for air carriers (reported to NTSB)
- 10% of air carrier turbulence related accident resulted in damage to the aircraft
- Causes aircraft fatigue and shorter airframe life
- Second leading weather factor affecting air traffic controller workload



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Motivations (cont.)

- Incidentally...
 - For 2022: 17 injuries, 13 crew or 76% (NTSB)
 - Est 4500/year
 - Most not wearing seat belts...
 - Large fraction due to convection
 - Kaplan et al. (2005) found 38 of 44 of severe turbulence encounters were in or near convection
 - Wolff and Sharman (2008) found about 40%
- Requirements for better turbulence
 avoidance from
 - FAA
 - ICAO (International Civil Aviation Organization)

Avianca Airlines Lima to Buenos Aires over Andes at 41,000ft 23 passengers and cabin crew members injured.

Extreme turbulence Aeroflot Moscow-Bangkok light 2353 UTC 30 Apr 2017 B777 at FL350 (238

"Aircraft scale turbulence"="fine-scale"



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Nature of turbulent events



Fine scale



Continuous peak EDR 20.1

Aviation turbulence intensity

- Traditionally based on Pilot Reports (PIREPs/AIREPs)
 - Subjective opinion of pilot "none"

"light"

- "moderate" (>1/2 g) may avoid
- "severe" (>1 g) must avoid
- "extreme" (>2 g) must avoid
- Depends on the aircraft
- Moderate or greater (MOG) is an extremely rare event
 - ~1%

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- "severe" <~ 0.1%</p>
- Not atmospheric intensity metric
- Better to use energy dissipation rate ϵ or EDR= $\epsilon^{1/3}$ m $^{2/3}s^{-1}$
 - ICAO standard
 - Can relate EDR to aircraft loads (peak g $\sim \sigma_g \sim \epsilon^{1/3}$)
 - Convenient scale 0-1



Aviation turbulence climatology based on PIREPS



MOG/Total

15 years of FOS pireps (1993-2007)



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Aircraft in situ edr estimates

- NOAA AMDAR archive contains winds, T, qv on many aircraft at different observation frequencies
- Also have estimates of EDR from selected aircraft (DAL, SWA on AMDAR) – others are proprietary
- NCAR archive ~ 2000 ac from DAL, SWA, UAL, SWR, AAL; ~5x10⁴ counts/day DAL, SWA
- 1 min sampling rate recording peak and mean EDRs but reporting/downlink frequency depends on airline
 - Communication costs are an issue
 - Airline nervousness about litigation
- Algorithm included on all new Boeing aircraft and also available for new Airbus aircraft
- IATA (International Air Transport Association) developing database to include all airlines (available for a fee!)





Zovko-Rajak et al. MWR 2019

Aircraft in situ edr estimates – algorithm*

- Accesses ~ 8 Hz avionics data from onboard computer (e.g. Aircraft Conditioning and Monitoring System ACMS)
- Compute spectra of w, 80 samples/spectrum
- Assume spectra follows k^{-5/3} in 0.5-3.5 Hz frequency region
- Sliding 10 sec window with 5 sec overlap
- Within each window get best fit to k^{-5/3} (Smalikho 1997)
- -> 12 EDRs/min
- Average and peak EDR levels recorded every minute (~12 km) from the 12 EDRs
- Rigorous QC applied
- Average and peak are binned at 0.02 EDR intervals





*Sharman et al. JAMC 2014



In situ edr estimates: caveats

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- In situ verification exercises
 - Compare to accelerometer based methods from same aircraft
 - Simulations
 - Compare to von Karman turbulence simulation with known EDR and length scale (Frehlich et al., JAM 2001)
 - Use 2DOF response model to compute • EDR and compare to input
- Caveats
 - Statistics contain an unknown avoidance bias
 - Daytime bias
 - Does not provide source (MWT, cloud)
 - Limited to <45,000 ft (lower stratosphere)
 - Some discrete events may not follow -5/3 assumed distribution (Rodriguez Imazio, JGR 2023)
 - Does not have to be perfect Mainly need to distinguish between "smooth" and "moderate"
 - 0.02 EDR binning is adequate, 0.1 used on previous versions



Input EDR

10.000 realizations of a von Karman turbulence wind field with known edr (Sharman et al. **JAMC 2014**)



Other observations

- PIREPS
 - Must convert to EDR
 - Large position uncertainty (50% off by more than 23 km)
- AMDAR Ude
 - Must convert to EDR (Lee et al WAF 2022)
- ADS-B (Automatic Dependent Surveillance- Broadcast)
 - Use vertical rate converted to EDR
 - High density ~150,000 as of June 2022
 - No downlink costs
 - Challenging due to low sampling rate (~1Hz) and data quantization (e.g. ~0.3 m/s vertical rate)
 - Current research area at NCAR (L. Cornman PI)







Other observations (cont.)

- HVRRD
 - Infrequent (2x day), sparse
 - But
 - Does include stratosphere
 - Does provide vertical distribution -> N² and shear
 - Which aircraft observations do not
 - Coming need for turbulence forecasts in Upper Class E air space (>60,000 ft) for UAS, military, SSTs, etc.
 - Ko et al. JGR 2023 showed EDR statistics were consistent for HVRRD derived EDR and in situ aircraft derived EDR in overlapping regions:
 - Both show occurrence frequency for mean MOG is very small
 - Data fit well by log normal





Aviation Turbulence Forecasting Approach

- Seek operational aviation turbulence forecast model
- "Aircraft scale" eddies that affect aircraft ~ few meters to couple km (smaller for UAS)
- Aircraft response is aircraft dependent but this is what pilot reports: "light", "moderate", "severe"
- CANNOT forecast these levels for every aircraft in the airspace
- Instead need to forecast atmospheric turbulence measure (i.e. aircraft independent measure)
 - We forecast EDR (= $\epsilon^{1/3}$ m $^{2/3}$ s⁻¹)
 - For reference ICAO standard thresholds (2001) for mid-sized aircraft are
 - EDR=0.10, 0.3, 0.5 for "light", "moderate", "severe", resp.
 - We use EDR=0.15,0.22,0.34 m^{2/3}s⁻¹



Approach (cont.)

- No option to directly forecast globally or even regionally at say 25 m grid spacing operationally
- At lower resolutions current turbulence parameterizations don't work very well, esp. at upper-levels
- Use operational NWP model (e.g., WRF-RAP, HRRR, GFS)
- Compute "turbulence diagnostics" (D) from NWP output
- Assumes linkage between NWP resolvable scales and aircraft turbulence scales
- Ds are typically related to model spatial variations

For example: Ellrod Index=Deformation X shear

$$I = DEF S_{V}, \quad S_{v} = \left| \frac{\partial \vec{u}}{\partial z} \right|, \quad DEF = \left(D_{SH}^{2} + D_{ST}^{2} \right)^{1/2}$$
$$D_{SH} = \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \qquad D_{ST} = \frac{\partial u}{\partial x} - \frac{\partial v}{\partial y}$$



Approach (cont.)

- Multiple causes require multiple forecasting strategies →
- Graphical Turbulence Guidance (GTG)*
- Compute suite of turbulence diagnostics (D) converted to EDR (D*)
- GTG = ensemble weighted mean $GTG = W_1D_1^* + W_2D_2^* + W_3D_3^* + \dots$
- Ws and D*s are turbulence source and altitude dependent
- PBL, troposphere, stratosphere separately
- GTG=MAX(GTG CAT + GTG MWT + GTG CIT) EDR, all separately available

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- Operational
 - Currently available 24x7 on Operational ADDS (<u>http://aviationweather.gov/adds</u>)
 - Uses WRF-RAP NWP model updated hourly
 - Global on WAFS (GFS and UKMO), ECMWF updated every 6 hrs





0.00 0.140 0.310 0.540 0.800

*Sharman et al. Weather & Forecasting 2006

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Example GTG diagnostics – GTG/RAP FL390

20160309 i18 f006 WRF-RR

422 DEFSQ - remap option 2

20160309_i18_f006_WRF-RR

06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016

*439 CTSQ/Ri - remap option 2 06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016

N=139 edrt= 0.22 R= 10.0 rmse= 0.174 PODY,N,TSS,bias= 0.818 0.472 0.290 2.515

N=139 edrt= 0.22 R= 10.0 rmse= 0.138 PODY,N,TSS,bias= 0.394 0.557 -0.049 1.818

 20160309_118_006_WRF-RR
 14-JUN-16

 *404 Elirod2 - remap option 2
 06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016

 N-139 edrt
 0.22 R = 10.0 mse= 0.170 PODY.N.TSS.bias= 0.758 0.509 0.267 2.333



20160309_118_006_WRF-RR 14-JUN-16 *433 EDRLL - remap option 2 06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016 N-139 edrt - 0.22 R= 10.0 ms= 0.137 PODY.N,TSS bias= 0.333 0.594 -0.072 1.636



20160309_i18_1006_WRF-RR 14-JUN-16 *453 wsq/Ri - remap option 2 06-hr turbulence forcesat at FL390 Valid 0000 UTC Wed 10 Mar 2016 N-139 edre 0.22 R= 10.0 mse- 0.100 PODV NTSS bias= 0.000 0.925 - 0.075 0.242



20160309_118_1006_WRF-RR 14-JUN-16 *415 NGM1 - remap option 2 06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016 N-139 edrt - 0.22 R= 10.0 mse= 0.120 PODY.N_TSS.bias= 0.727 0.660 0.388 1.818



20160309_i18_1006_WRF-RR 14-JUN-16 *435 1/RiTW - remap option 2 06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016 N=138 ordr. 02 2 R = 10 0 mse. 0 155 PODY N TSS biase. 0 212 0 604-0 184 1485



 20160309_118_1006_WRF-RR
 14-JUN-16

 *456
 SIGW/RI - remap option 2

 06-hr turbulence forecast at FL390
 Valid 0000 UTC Wed 10 Mar 2016

 N-139 edrt
 0.22 R= 10.0 msg-e

 0.139 PODY.NTSS.bias=
 0.121



 20160309
 j18_1006_WRF-RR
 14-JUN-16

 *458
 F2D/Ri - remap option 2
 06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016

 N=138 edric 0.22 R= 10.0 msg= 0.147 PODY.MTSS.bias= 0.788 0.481 0.269 2.455
 0.289 2.455



20160309_118_006_WRF-RR 14-JUN-16 *423 VORTSO/Ri - remap option 2 06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016 N=139 edite_ 0.22 R = 10.0 msse_ 0.181 PODY N.TSS.bias_ 0.727 0.557 0.284 2.152

14-JUN-16

14-JUN-16



 20160309_118_1006_WRF-RR
 14-JUN-16

 *441 iswind/R1 - remap option 2
 06-hr turbulence forecast at FL390 Valid 0000 UTC Wed 10 Mar 2016

 N-139 ødre
 0.22 R= 10.0 mseo
 0.128 PODY.NTSS.bias=
 0.879 0.566
 0.445 2.273







NCAR RESEARCH APPLICATIONS

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- Machine learning (ML)
 - Avoids some of the calibration issues
 - But requires large amounts of observational data for training
 - Initial results are encouraging (Muñoz-Esparza et al. 2020, Kaluza)



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- Probabilistic approaches
 - Multiple diagnostics as an ensemble (MDE)
 - Multiple NWP ensembles (FME)
 - Time-lagged NWP output (TLE)
 - Some combination (Shin et al. WAF 2023)



Muñoz-Esparza et al. 2020

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RESEARCH APPLICATIONS

LABORATORY

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Muñoz-Esparza et al. 2020



GTG verification: sample results

Develop verification metrics from many cases

- Compare observation to GTG surrounding grid points
- Use in situ "peak" EDR (~1 km uncertainty)
- Compute skill statistics to evaluate diagnostics/suite
 - MAE, RMSE, bias, ROC curves (Kaluza presentation)...
 - Discrimination ability
 - Cannot distinguish between NWP and diagnostic errors
 - All show deterministic ensemble mean has superior skill to individual diagnostics





Summary

- Semi-empirically based diagnostics can provide operationally useful forecasts of CAT and MWT using coarse resolution NWP model output
 - For aviation, $\varepsilon^{1/3}$ =EDR is preferred observation/forecast metric
 - Using an ensemble of turbulence diagnostics instead of one diagnostic gives more robust statistical performance
 - Could also be used with an ensemble of NWP models
 - ML techniques show promise
 - Ultimately, approach must be probabilistic
 - CIT (convectively-induced turbulence) is challenging -> must nowcast
- Use of in situ EDR data allows more reliable tuning and verification
- HVRRD is useful to compare statistics of observational data, esp. in stratosphere

Longer term research needs

- Need better understanding of causes and lifecycles of turbulence
 - What are the sources/damping mechanisms?
 - What is the role of inertia-gravity waves, breaking, Ri reductions?
 - What is the role of the tropopause and tropopause folds?
 - How to handle wave-turbulence interactions?
 - Establish turbulence current and future climatology (P. Williams talk)
 - Need dedicated multiple aircraft field programs (dropsondes + penetrations)
- Modeling
 - What is "optimal" resolution for turbulence forecasting?
 - Need better subgrid turbulence parameterizations in free atmosphere -> ε
 - Nested simulations that include large (forcing) scale plus smaller scale have been highly successful
 - Need more cases based on accidents, elevated edr data
 - Need resolution, parameterization, initialization sensitivity studies

Many good PhD topics here!! For more see Sharman, Lane, Schumann (2017)